

STUDY OF WELL BARRIER HOLE BURNING IN QUANTUM WELL BISTABLE LASERS

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ABSTRACT

Quantum carrier capture and release effects on optical bistability in multiple quantum well (MQW) lasers are studied using the well barrier hole burning model. The ratio of carrier capture to release time (η) is varied and the hysteresis width, transient behavior are analysed by simulating the equivalent circuit of MQW bistable laser using circuit simulation program Pspice. The hysteresis width is found to increase with an increase in η . From the time response, improved damping and increased turn on delay are observed in switching characteristics for higher value of η .

Keywords: Multiple quantum wells, well barrier hole burning, semiconductor lasers, bistability, hysteresis, circuit modeling

INTRODUCTION

Optical bistability in semiconductor lasers has received much attention because of its potential application in optical switching and signal processing. It is well established that the presence of an unpumped absorber in the laser cavity can lead to bistability. Introducing quantum wells in the active regions of gain and absorber sections could significantly improve the switching speed and controllability of hysteresis characteristics [1]. It is also found that the conventional single mode rate equations fail to explain the resonance characteristics profoundly, because of non inclusion of factors such as spatial and spectral inhomogenities. Hence well barrier hole burning model is introduced to incorporate the effects contributing to non linear gain [2,3]. MQW bistable lasers are normally analysed by numerically solving the single mode rate

MQW bistable lasers using circuit simulation technique. Circuit simulation method is adopted because of its advantages, such as inclusion of parasitics and device- circuit interactions [4]. The equivalent circuit is also vital for the design of control and driver circuits for laser [5]. The equivalent circuit is simulated for dc sweep and transient conditions using circuit simulation program Pspice.

LARGE SIGNAL MODEL

The bistable laser has two regions viz. gain and absorber sections. For the simulation purpose, we have considered InGaAs - InAlAs MQW structure. This structure consists of 6 quantum wells in the active region having 5 ps capture time. The carrier lifetime in the barrier and in the well is 1ns. The carrier lifetime in the gain section is assumed to be proportional to the carrier density, whereas it is constant (2ns) in the absorber section. The non linear rate equations incorporating well barrier hole burning [2] are included in the gain section of the bistable laser. Since the absorber section is unpumped, the carrier transport and capture effects are neglected. The above modifications are made in the rate equations of ref [1] and given as

$$\frac{dN_b}{dt} = \frac{J}{e d} - \frac{N_b}{\tau_{sb}} - \frac{(N_b - \eta N_w)}{\tau_c} \quad (1)$$

$$\frac{dN_w}{dt} = \frac{e d \tau_{sb}}{(N_b - \eta N_w)} - \frac{N_w}{\tau_c} - v_g G_g S \quad (2)$$

$$\frac{dN_a}{dt} = - \frac{N_a}{\tau_a} - v_g G_a S \quad (3)$$

equations [1]. In this paper, we have attempted to study the effect of well barrier hole burning in

$$\frac{dS}{dt} = \xi (1-h) v_g G_g S + \xi h v_g G_a S + \beta \xi (1-h) \frac{N_w}{\tau_{sw}} - \frac{S}{\tau_p} + P_{in} \quad (4)$$

where N_b , N_w and N_a denotes the carrier density in the barrier layer, well region in gain section and absorber section respectively. The rate of gain (absorption) in the gain and absorption regions, G_g and G_a are approximated by a linear function of carrier density [1]

Multiplying the eqns (1)(2)(4) by qV_g and (3) by qV_a and rearranging one gets

$$I = I_{D1} + \frac{\tau_{sw}}{\tau_{sb}} \frac{dI_{D1}}{dt} + \frac{\tau_{sb}}{\tau_c} I_{D1} - \eta \frac{I_{D2}}{\tau_c} \quad (5)$$

$$\frac{\tau_{sb}}{\tau_c} I_{D1} = \frac{\tau_{sw}}{\tau_c} \frac{dI_{D2}}{dt} + \eta \frac{I_{D2}}{\tau_c} + I_{D2} + I_{stg} \quad (6)$$

$$\frac{dI_D}{dt} = -I_{D3} - I_{sta} \quad (7)$$

$$C_p \frac{dP}{dt} = \xi (1-h) I_{stg} + \xi h I_{sta} + \beta \xi (1-h) I_{D2} - \frac{P}{\tau_p} + P_{in} \quad (8)$$

TABLE I

Fig.1

Fig.2

Fig.3

where $qV_g N_b / \tau_{sb} = I_{D1}$, $qV_g N_w / \tau_{sw} = I_{D2}$,
 $qV_a N_a / \tau_a = I_{D3}$ being the spontaneous
emission
terms included as diode currents.

$$I_{stg} = qV_g V_g g_g (N_w - N_{og}) (1 - \epsilon S)$$

$$I_{sta} = qV_a V_g g_a (N_a - N_{oa}) (1 - \epsilon S)$$

are the recombination currents caused by
stimulated emission in the gain and absorpction
region respectively.

$$C_p \frac{dP}{dt} = qV_g \frac{dS}{dt}, \quad C_p = qV_g S_N$$

and $\tau_p = R_p C_p$. S_N is the normalisation
constant. The values of the parameters used are
given in Table.I

Combining eqns (5) - (8), the large signal
equivalent circuit is developed as shown in
Fig.1. The modeling approach is similar to the
large signal model for bistable lasers [6].

SIMULATION RESULTS

The equivalent circuit is simulated for dc sweep
and transient conditions using circuit simulation
program Pspice. The simulations are carried out
without any external optical injection. (P_{in} equals
zero) and τ_{sw} is given the same value as τ_{sb} .
The dc simulation shows hysteresis which
validates our proposed model. The simulation is
done for different values of η . It is found that the
threshold current and hysteresis width increase as
 η increases. The hysteresis characteristics are
shown in Fig.2. In the transient simulation, the
device is biased near the threshold and an
electrical pulse of 10 mA amplitude and 1 ns
width is given to the gain section and the
switching characteristics are observed. In the
time response (Fig.3), the turn on delay and
steady state amplitude are found to increase
with η . Further, the damping becomes large
(reduced relaxation oscillations) as η increases
and makes the switching transition smooth.

CONCLUSION

Well barrier hole burning effects are studied in
MQW bistable laser diodes by simulating the
equivalent circuit incorporating well barrier hole
burning model. The hysteresis width and
threshold current are found to increase with
capture ratio η . Increased damping and turn on
delay result for higher η , which is observed from
the transient response.

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TABLE I

Parameter	Description	Value
V_g	Volume of gain section	$4.69 \times 10^{-11} \text{ cm}^3$
V_a	Volume of absorber section	$1.62 \times 10^{-12} \text{ cm}^3$
N_w	Number of wells	6
L_w	Well thickness	90 Å
L	Length of laser cavity	300 μm
L_g	Length of gain section	280 μm
g_g	Gain constant of gain section	$1.69 \times 10^{-6} \text{ cm}^3 \text{ s}^{-1}$
g_a	Gain constant of absorber section	$3.38 \times 10^{-4} \text{ cm}^3 \text{ s}^{-1}$
τ_{sb}	Carrier lifetime in barrier	1 ns
τ_{sw}	Carrier lifetime in well	1 ns
τ_c	Capture time	5 ps
τ_a	Carrier lifetime in absorber	2 ns
τ_p	Photon lifetime	1.87 ps
N_{og}	Transparency carrier density in gain section	$1.25 \times 10^{18} \text{ cm}^{-3}$
N_{oa}	Transparency carrier density in absorber section	$1.15 \times 10^{18} \text{ cm}^{-3}$
ϵ	Gain compression factor	$2 \times 10^{-17} \text{ cm}^3$
ξ	Optical confinement factor	0.15
β	Coupling coefficient	1×10^{-5}
v_g	velocity of light in medium	$8.45 \times 10^9 \text{ cm s}^{-1}$
R_s	series resistance	5 Ohms
L_{pp}	lead inductance	1 nH
C_{pp}	parasitic capacitance	1 pF
R_{in}	source resistance	1000 Ohms
C_D	diffusion capacitance	10 pF
S_N	normalisation constant	10^{15}
h	ratio of saturable absorption region to cavity length	0.03